

Introduction to Power Transformer Testing

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ALTANOVA, a Doble Engineering Company, provides diagnostic solutions to utilities and industries to improve the performance of their electrical assets through portable testing equipment, advanced monitoring systems, and professional services.



Altanova History



I.S.A. Istrumentazioni Sistemi Automatici S.r.l. is established in Taino ITALY

1999 TECHIMP was born as a spin-off from the University of Bologna ITALY.

- 1.S.A. and TECHIMP merge giving birth to the ALTANOVA GROUP
- 2019 INTELLISAW joins ALTANOVA GROUP

2021

1938

ALTANOVA GROUP becomes part of ESCO Technology Group and joins the Doble Engineering Company, as part of the USG division.





Altanova Today















PRODUCT BRANDS



Our Solutions

Electrical Test Equipment

Essential for day-to-day maintenance tests of electrical assets. Useful in specific phases of the asset lifecycle:

- Procure
- Operate
- Maintain
- Decommission.

Professional Services

Diversified offer according to the electrical asset lifecycle:

- Installation and commissioning
- Diagnostic test
- Data analysis
- Consultancy
- Training.





Monitoring Systems

Shift from a time-based maintenance to a condition-based maintenance.

Focus on predictive maintenance and shift in focus from electric asset value cost to network outage costs.

Strong evolution of digitalization trend in the power industry.

Power transformers Current & voltage transformers **Circuit breakers** Protective relays HV gas insulated switchgears Meters and transducers MV/HV/EHV cables Rotating machines MV/LV switchgears Variable speed drives **Overhead** lines Batteries

Testing And Monitoring Solutions For:





TRANSFORMER

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Transformer



1830s - Joseph Henry and Michael Faraday works with electromagnets and discover the property of induction independently on separate continents.



Faraday's Experiment - RELATIONSHIP BETWEEN INDUCED EMF AND FLUX

Transformer



What is a Transformer ?

A transformer is a device that transfers electrical energy from one circuit to another through inductively coupled conductors, the transformer's coils/



Working of Transformer

- Transfer of electric power from one circuit to another.
- Transfer of electric power without any change in frequency.
- Transfer with the principle of electromagnetic induction.
- The two electrical circuits are linked by mutual induction





Why do we need Transformer

- To step-up and step down the voltage.
- Need for transmitting power from one place to another.
- For isolating and Protection of the circuit.









Transformer Main Parts



- Core
- Winding & Insulation System
- Tap Changer OLTC
- Tank
- Bushings
- Radiator

- PRV Pressure Relief Valves
- Conservator
- Breather
- Marshalling Box
- BUCHHOLZ Relay
- OSR Oil Surge Relay
- Temperature indicator

Transformer - Core

- The role of the magnetic core is to increase and concentrate the magnetic flux that links the primary and secondary coils.
- It is made up of thin laminations of CRGO of thickness 0.28 mm to 0.35 mm.
- Laminations are insulated from each other by oxide coating.
- Magnetostriction in the core produces a vibration that causes audible noise called as Humming (due to contract and expansion of core material)







Transformer - Core

- It is the backbone of the transformer from magnetic and mechanical aspect.
- It provides a path for Magnetic flux.
- It supports windings.
- Low losses, better heat dissipation, low vibrations.
- Higher working flux, specific core losses W/Kg at peak flux density 1.7 Tesla at 50 Hz, ageing withstand capability.







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Transformer – Windings & Insulation System

- Windings are made up of Copper material.
- Wound concentrically around the core limbs.
- LV winding with thick cross sectional area is placed near the core on the press board cylinder.
- HV winding is placed above LV winding and is separated by press board cylinder and by oil ducts, hence HV winding is away from the core.





Transformer – Windings & Insulation System



- Superior Craft Paper Insulation is wrapped over conductor.
- Most sensitive part subjected to Thermal, Mechanical and di-electric Stresses.
- Major Insulations used in Windings are Thermally upgraded Craft Paper Cylinders, Synthetic Resins bonded press board cylinder and press board sheets.
- Minor Insulations used in windings are Press Board spacers, Cellulose tape and synthetic enamel wire.



Transformer – Windings & Insulation



Transformer – Tap Changer

- Responsible of Tap Changer is :
 - 1. To supply a desired voltage to the load
 - 2. To counter the voltage drops due to loads
 - 3. To counter the input supply voltage changes on load
- There are Two types of Tap Changer No load (De-energized) Tap Changer – NLTC/DETC On Load Tap Changer - OLTC



Transformer – Tap Changer

- On Load Tap Changer is mounted vertically within the Transformer Tank.
- It consists of diverter switch and Tap selector and separate Driving Mechanism Box.
- Driving Mechanism Box is fitted on the side of the Transformer Tank.





Transformer – On Load Tap Changer





Selector Switch Contact with Roller Contact



Diverter Switch Contact

Transformer – Tap Changer



Tap Changer



Transformer - Tank



- It is made from Steel material.
- Fabricated welded construction to obtain a box type construction.
- Supports and encloses various parts.
- Should be strong sturdy, free from vibrations.



Transformer - Tank



- Should withstand mechanical load during handling, lifting and transport
- Should withstand Vacuum test and Pressure test
- Tank cover supports, tap changers and other fitments.
- It's accessories includes lifting legs, manhole for inspection, valves for filling and draining oils, earthing terminals.
- Contains filling pipes (to fill in the oil)
- Also lifting bolts to position it into place





- Bushing is designed to withstand the electrical field strength produced in the insulation
- Provides insulated support to conductor connecting the external terminal to the Transformer winding
- The leads of HV and LV windings are brought out and connected to the terminals of the Bushings.





- How to recognize the HV from LV bushings – HV are longer and have more ribs (due to higher voltage) – also in most of the cases has tap adapter – a measurement point for TD (PF,DF) and PD measurement
- LV bushings are shorter but the conductor there is thicker due to the higher current





- Bushing mounted vertically or inclined on tank over on turrets.
- Two most common type of bushing are
 - solid porcelain bushings onsmaller transformers
 - oil-filled condenser bushings on larger transformers
- From the physical and electrical point of view, bushing appears to be the weakest part of the transformer.









Current creates big electrical field – which in turn ionizes the insulators and produces a leakage current.

Big Leakage current – Could cause flashover

We want a small leakeage current that is why we make the path of a leakage current longer with «ribs» on the bushing.

Also the ribs allow the bushing to keep some parts of the bushing dry when it is raining – to have lover leakage current



Transformer - Radiator



- The **radiator of transformer** accelerates the cooling rate of transformer.
- Oil immersed transformer is always provided with radiator.
- Plays a vital role in increasing loading capacity of an electrical transformer.
- Increases the surface area for dissipating heat of the oil.
- Oil immersed power transformer is generally provided with detachable pressed sheet radiator with isolating valves.



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Transformer - Radiator



In case of Small size distributing transformer, the radiators are generally integrated parts of transformer body and projected from the main tank.



Transformer - Radiator



Operation:

- Under loaded condition, warm oil increases in volume and comes to the upper portion of the main tank
- Then this oil enters in the radiator through top valve and cools down by dissipating heat through the thin radiator wall.
- This cold oil comes back to the main tank through the bottom radiator valve.
- This cycle is repeated continuously till the load is connected to the transformer.
- Dissipation of heat in the transformer radiator can be accelerated further by force air provided by means of fans.



Transformer – Pressure Relief Valve(PRV)

- Pressure Relief Valve is a safety element of the transformer
- PRV prevent heavy damages of the tank in the case of sudden rise of the internal pressure
- Designed in order to remove the excess pressure in a very short time as soon as pressure limit exceed
- During fault this PRV operate and trip the transformer, so it can be protected from further damage



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Transformer - Conservator



- Conservator is a cylindrical tank mounted on supporting structure on the roof of the transformer main tank
- Provides adequate space to the expanded transformer oil
- Acts as a reservoir for transformer insulating oil
- In normal conditions filled up to about 50 %







Transformer - Breather



- Breather is used to absorb moisture in air while breathing
- A silica gel breather is the most commonly used way of filtering air from moisture
- Silica gel breather for transformer is connected with conservator tank by means of breathing pipe
- As silica gel becomes more affected by moisture, its colour changes
- There are few approaches here blue to white and vice versa


Transformer - Marshalling Box

- Marshalling Box is the master control panel for the protection devices.
- Marshalling box shall be provided with terminals for:
 - oil temperature indicator,
 - winding temperature indicator,
 - magnetic oil gauge
 - and buchholz relay.
- Marshalling box shall be weather proof type and shall be provided on the front side of transformer tank
- All the secondary wiring of the transformer from current transformers are terminated at the Marshalling Box .



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Transformer – Buchholz relay



- Buchholz relay in transformer is an oil container housed on the connecting pipe from main tank to conservator tank.
- It is mechanically Actuated.
- Gasses produced, due to internal faults, are the cause of actuating the upper switch of the relay.
- Surge of oil, due to severe faults (phases short circuit), strikes the baffle plate and close the mercury switch of the lower element.



Transformer – Buchholz relay







Transformer – Oil surge Relay



- The OSR (Oil Surge relay) is located on the OLTC (On load tap changer) chamber
- Principal of OSR relay is similar to the Buchholz relay
- As we know, OLTC has Moving parts and here more sparking come in picture due to which gas pressure builds up in OLTC chamber, this pressure is sensed by the OSR and the OSR trips the circuit





TRANSFORMER FAILURE

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Transformer Failure



- Is inevitable if transformer is not taken care of
- Is exactly what we would like to avoid by properly maintaing the PT in good health



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Important questions to ask ourselves

- Why test ?
- When to test ?
- Who should test ?
- What tests ?



Important questions to ask ourselves 🏠 Why test ?

Because transformers are:

- Expensive
- Usually reliable and durable
- Faults can and do sometimes occur
- Difficult to diagnose
- Maintenance and visual inspections limited value
- Often uneconomic to repair
- Failures can be catastrophic
- Appropriate monitoring and management policies



Views on testing



'We don't have any problems, So we don't do any testing'

'When we get a failure, The first question the boss asks is "WHEN WAS IT LAST TESTED ?"



An Appropriate Policy?





'If it ain't broke, Don't fix it'

Condition based methodology When to test ?



Every 3 to 5 years if there are no issues with PT

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Visual Inspection





Important questions to ask ourselves

Who should do the testing ?

- University researchers
- Test equipment manufacturers
- Transformer manufacturers
- Utility maintenance personnel
- Service companies





RECOMMENDED TESTS ON POWER TRANSFORMER

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Recommended Tests on Power Transformer



- Ratio / Vector Group
- Winding Resistance and Dynamic Resistance Measurement
- No Load Test/Exciting Current
- Short Circuit Impedance (Leakage reactance) and Frequency Response to Stray Losses
- Insulation Resistance (DC method)

- Tangens Delta (Power Factor, C&DF Dissipation Factor) (AC method)/ Tip up and Tip down Tan Delta/Variable frequency Tan Delta
- SFRA Sweep Frequency Response Analysis
- Partial Discharge Test
- Oil tests (DGA, breakdown voltage)



TRANSFORMER TURNS RATIO (TTR) TEST



The **turns ratio** is defined as the ratio of the number of turns of wire in the primary winding (NP) to the number of turns of wire in the secondary winding (NS)





Also the turn ratio (N) can be defined as the no-load voltage ratio between two windings of a transformer.

This test can be done on lower voltage levels – for example up to 200 V or Higher voltage levels – for example 10 kV – LV and HV TTR

The HV TTR requires more advanced test sets, but can uncover more issues as it stresses more the insulation



 $N = V_P / V_S$



Purpose of Turns Ratio Test:

- Identify if there is:
 any shorted Turns,
 - any Open turns in HV winding.
- Provides Information on insulation failure between turns.
- Helps in Identifying the Vector Group of the Transformer.





Example - Instruments Required to Test :

AC voltage Source and Voltage Measurement input, like STS 5000.









Before Test:

- Need to know:
 - Type of Transformer
 - Number of winding
 - Phases
- Voltage Applied:
 - Must not exceed the Rated Voltage of Transformer
 - Always to the HV side of the Transformer
- Voltage Measured:
 - Must not exceed the measurement input of the Voltmeter.
- Turns Ratio
 - Must be measured on all Taps.





Testing on a single Phase Transformer







Ratio Measurement on a Single Phase Transformer





Ratio Measurement on a Single phase Auto Transformer





Transformer Turns Ratio Plot wrt Tap



Turns Ratio



Ratio of Three Phase Transformer

- Three phase transformer consists of three sets of primary windings, one for each phase.
- Three sets of secondary windings wound on the same iron core.





220kV Three Phase Transformer





Transformer Ratio test on a YNyn0 Vector Group





Transformer Ratio test on a YNd11 Vector Group





Transformer Ratio Test using Switch Box

- One time connection
- Automatic control of OLTC
- Perform the test as per the Vector Group mentioned
- Also possible to use an integral solution test set with integrated switchbox







Test Result of Ratio Test on 400kV Transformer



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Transformer Turns Ratio (TTR)

For the ones who want to know more - current measured is actually No Load current

		Vn HV [V]	V HV [V]	I HV [A]	φI HV [°]	V LV [V]	φV LV [°]	Ratio	Err %	
	Α	200,0	201,7	2,136m	69,5	74,722	-31,0	2,6993	0,21	C
V	В	200,0	201,7	1,554m	69,4	74,633	-31,0	2,7023	0,32	C
V	С	200,0	201,7	2,006m	68,8	74,555	-40,0	2,7051	0,43	C

		Vn HV [V]	V HV [V]	I HV [A]	φI HV [°]	V LV [V]	φV LV [°]	Ratio	Err %	
	Α	200,0	201,6	2,124 m	68,6	73,445	-30,0	2,7455	74,64m	0
V	B	200,0	201,6	1,544m	68,4	73,357	-30,0	2,7487	0,19	0
V	С	200,0	201,6	2,024 m	68,6	73,269	-31,0	2,7517	0,30	0

		Vn HV [V]	V HV [V]	I HV [A]	φI HV [°]	V LV [V]	φV LV [°]	Ratio	Err %	
	Α	200,0	201,5	2,360m	68,5	61,077	-26,0	3,2995	0,22	0
7	В	200,0	201,5	1,761m	68,8	60,989	-26,0	3,3043	0,37	0
	С	200,0	201,5	2,277m	68,2	60,892	-25,0	3,3094	0,52	0

Result evaluation - ratio error < 0.5 %

Tap 1

Tap1



Test Result of Ratio Test on 104 kV Transformer

	Tap #			Ratings		Vector Group		Phases		
HV				104,000 kV	D	-	3-	ohase 💌		
LV		2L	•	22,900 kV	yn	• 1				
		т	um ratio	7,866						
est	valu	ies		STCS						
				Auto-tap	OLTC	•	current 2L	•		
Fest	Volta	age	200,0 V	Pulse time	4,	0 s	from 2R	•		
Test	Freq	luency	60,0 Hz	Auto-phase	ABC	•	22			
Rest	ılts									
		Vn HV [V]	V HV [V]	I HV [A]	ΦI HV[°]	V LV [V]	ΦV LV[°]	Ratio	Err %	
	A	200,0	199,9	0,854m	64,3	24,957	-78,0m	8,0113	0,60	Ç
2	B	200,0	200,0	1,154m	63,0	24,959	-95,0m	8,0140	0,63	¢
-	C	200,0	200,0	1,099m	65,6	24,966	-97,0m	8,0116	0,60	C

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V HV [V] ΦI HV[°] V LV [V] ΦV LV[°] Vn HV [V] I HV [A] Ratio Err % 🗹 A 200,0 199,9 0,854m 24,957 8,0113 G 64,3 -78,0m 0,60 🗹 В 0,63 200,0 200,0 1,154m 63,0 24,959 -95,0m 8,0140 C 200,0 200,0 1,099m 65,6 24,966 -97,0m 8,0116 0,60 C

		Vn HV [V]	V HV [V]	I HV [A]	ΦI HV[°]	V LV [V]	ΦV LV[°]	Ratio	Err %	
	Α	200,0	200,0	0,993m	71,9	25,117	-88,0m	7,9632	0,62	0
V	B	200,0	200,0	1,303m	69,3	25,107	-84,0m	7,9659	0,65	0
	С	200,0	200,0	1,239m	69,5	25,111	-91,0m	7,9639	0,63	0

	Vn HV [V]	V HV [V]	I HV [A]	ΦI HV[°]	V LV [V]	ΦV LV[°]	Ratio	Err %	1
Α	200,0	200,0	0,884m	65,0	25,325	-0,1	7,8990	0,42	0
В	200,0	200,0	1,141m	62,1	25,318	-0,1	7,9010	0,44	0
С	200,0	200,0	1,049m	62,0	25,324	-77,0m	7,8981	0,41	0

		Vn HV [V]	V HV [V]	I HV [A]	ΦI HV[°]	V LV [V]	ΦV LV[°]	Ratio	Err %	1
	A	200,0	200,0	1,095m	70,1	25,486	-0,1	7,8486	0,39	0
~	B	200,0	199,9	1,394m	67,8	25,470	-87,0m	7,8504	0,41	0
~	С	200,0	200,0	1,334m	67,7	25,486	-0,1	7,8487	0,39	0

Result evaluation – ratio error < 0.5 %

Even thou we see error > 0.5%, it does not mean that we autmatically need to replace the PT. It means we need to investigate further more



Tap2

Tap 1

Tap 4



VECTOR GROUP TEST

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Vector Group Test



Connection of a 3 Phase Transformer

The vector group of transformer is an essential property for successful parallel operation of transformers.

- Eg: Dyn11
- "D" indicates delta 1ry winding.
- "yn" indicates Star with Neutral 2ry winding
- "11" indicate the difference in phase angle between the windings, with HV winding is taken as a reference. The number is in units of 30 degrees.

Selection of Phase in case of phase by phase measurement is very critical.


Vector Group Test



Two tests need to be executed in order to verify if the Vector Group is correct.

In both cases we need to short circuit phases B and C on the primary side and generate voltage between phases A and B on the primary side.

Test 1:

We measure on secodary side between phases A and B



Vector Group Test



Test 2:

We measure on secodary side between phases A and C

Automatically we get the result

Obtained vector group needs to be the same as the nominal vector group.





WINDING RESISTANCE TEST

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Winding resistance measurements in transformers are of fundamental importance for the following purposes :

- Calculations of the I^2R component of conductor losses.
- Calculation of winding temperature at the end of a temperature test cycle.
- As a Bench mark for assessing possible damage
- Last test to be executed (due to magnetisation of the core the same should be demagnetized before doing No Load and SFRA test)
- It is done at site in order to check for abnormalities due to
 - broken strands of conductor,
 - high contact resistance in tap changers,
 - high voltage leads and bushings in the field.
 - loose connections.



- Transformer winding contains inductance and Resistance
- The DC current source must be extremely stable.

$$V_{dc} = | R + L \frac{di}{dt}$$

= DC current through transformer winding
= resistance of the transformer winding
= inductance of the transformer winding
di/dt = changing value of current (ripple)

- The inductor current must not be allowed to jump instantaneously from one value to another.
- Note : Open-circuit a physical inductor through which a finite current is flowing, an arc will appear across the switch.
- The fact that we use DC current means that we measure Resistance not Impedance



Procedure

- For star connected winding, the resistance measured between the line and neutral terminal.
- For star connected auto-transformers, the resistance of the HV side is measured between HV and LV terminal, then between LV terminal neutral
- If OLTC Present, Resistance shall be taken at each Tap continuously without Discharging the Transformer
- If DETC Present, Resistance measured at each tap and before changing the Tap Transformer must be denergized
- For delta connected windings, between pairs of line terminals (A-B, B-C, C-A)
- Use Temperature Compensation ("recalculate" the measured values to the temperature at which the initial resistance measurement was done (usually around 70°C)

Test Requirement

- Stable DC current Source
- Voltmeter
- Algorithm for stable reading of the Resistance
- Discharging after Measurement
- It would be good if the testing current is not smaller than 1% of nominal current and not bigger than 10 %
- It can take time (few min) to initially charge the transformer core so that $\frac{di}{dt}$ change of current becomes 0
- Time (s)







Winding resistance test with STS 5000





Winding Resistance with Switch Box :

- Automatic Winding Resistance test on 3 Phase Transformer.
- Measurement is performed both at Primary and Secondary.
- Automatic Control of OLTC of the Transformer for testing of transformer at all Taps.
- It reduces the measurement time a lot (by 70 %) because each Ph is only once energised and de-energised so 3 time all together





Result evaluation – result needs to be within 2% of referece value (3% in some cases)

If reference values are not available – Phases are compared – again - 2 % difference between phases is max tolerance

Example 1 – Primary side resistance – usually higher resistance if we talk about step down Transformer (36.7 Ω)

Nominal values	Measure	Compensation —				
3-phase 🔻	C 10V	🔽 Temp. compens	ation Mat	erial	Cu	-
		C Fahrenheit [°F]	Amt	pient t.	25,	0 °C
Nominal resistance 36,000 Ω	• 300V	Celsisus [°C]		erence t.	40,0 °C	
Test values	STCS pre	sent				
Output Range 6A 👻	Auto-tap	None	•			
Test current 0,900 A						
Min R 5 556 m0						
5,550 HB2	2					
Max R 38,889 Ω	Auto-phase	ABC	-			
Results						
Data results Graphical representation	OLTC Graph (Do	own) OLTC Graph	(Up)		EX	port
Phase I test [A] I DC [A	A] V DC [V	/] Time [s]	R meas [Ω]	R comp [Ω]	R nom [Ω]	Error
🖌 A 🗾 0,900 0,	899 32,9	979 322,6	36,6642	38,8256	36,0000	2
A 0,900						
🖌 В 🗾 0,900 0,	899 33,0	274,3	36,7542	38,9208	36,0000	4
В 0,900						
✓ C 0,900 0,	898 33,1	164 277,6	36,9229	39,0996	36,0000	9
C 0,900						



Example 2 – Secondary side resistance – usually

lower resistance if we talk about step down

Transformer (0.63 Ω) because lower voltage on the trafo means higher current and for higher current we want lower resistance to reduce the losses.

Observe R_{meas} and R_{comp} colums (compensation)

Also see the difference in time needed to execute the measurement (Ph A 118 s vs. 22 s)

Measure Con	npensation					
C 10V	10V Temp. compensation		erial	Cu	Cu 🔻	
	Fahrenheit [°F]	Amt	pient t.	25,	0 °C	
• 300V •	Celsisus [°C]	Refe	erence t.	40,	40,0 °C	
STCS preser	it					
Auto-tap	None	•				
Auto-phase	ABC	•				
OLTC Graph (Down) OLTC Graph	(Up)		Ex	port	
A] V DC [V]	Time [s]	R meas [Ω]	R comp [Ω]	R nom [Ω]	Error	
,971 3,194	118,5	0,6430	0,6809	0,6000	c	
,981 3,205	22,0	0,6432	0,6812	0,6000	q	
,992 3,140	116,9	0,6289	0,6660	0,6000	q	
,002 3,145	23,8	0,6288	0,6658	0,6000	d	
,992 3,181	125,1	0,6374	0,6750	0,6000	d	
,015 3,198	24,9	0,6378	0,6754	0,6000	q	
	Measure Con 10V I 300V I Stress I Auto-tap I Auto-phase I 0LTC Graph (Down I 4,971 3,194 9,971 3,194 9,992 3,140 5,002 3,145 3,015 3,198	Measure Compensation ○ 10V ✓ Temp. compens ○ 300V ○ Fahrenheit [°F] ○ 300V ○ Celsisus [°C] ✓ STCS present	Measure Compensation ○ 10V Image: Temp. compensation Mat ○ 10V Fahrenheit [°F] Amt ○ 300V Ocelsisus [°C] Refe Image: STCS present Image: ABC Image: ABC Auto-tap None Image: ABC OLTC Graph (Down) OLTC Graph (Up) A V DC [V] Time [s] R meas [Ω] 4,971 3,194 118,5 0,6430 4,991 3,205 22,0 0,6432 4,992 3,140 116,9 0,6289 5,002 3,145 23,8 0,6288 4,992 3,181 125,1 0,6374 5,015 3,198 24,9 0,6378	Measure Compensation Material 10V Image: Temp. compensation Material Fahrenheit [°F] Ambient t. 300V Celsisus [°C] Reference t. Image: Temp. compensation Reference t. Image: Temp. comp. compensation Reference t.	Measure Compensation 10V Temp. compensation Material Cu Fahrenheit [°F] Ambient t. 25, 300V Celsisus [°C] Reference t. 40, STCS present Auto-tap None Mone OLTC Graph (Down) OLTC Graph (Down) OLTC Graph (Down) OLTC Graph (Up) Ex Alto-tap ABC Structure Time [s] R meas [Ω] R comp [Ω] R nom [Ω] Structure Structure	



Graphical presentation of Winding Resistance on each Tap





DYNAMIC RESISTANCE OF OLTC (Ripple & Slope of OLTC)

OLTC Contains :

- Diverter Switch
- Selector Switch







OLTC inside the Transformer Tank











Flow of current with time with change in time





Static resistance Provides values of:

All internal contacts (gives information of Selector Switch of OLTC)

+ dina Decista

Winding Resistance

All Internal Contacts contain :

- diverter switch contacts
- tap selector switch
- Internal Contacts



Static resistance with Ripple and Slope Provides values of:

All internal contacts + Winding Resistance + Information on Dynamic movement of Diverter Switch

Note : Test is always performed for both up ward movement and downward movement of tap position.

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NO LOAD CURRENT (Excitation Current Test)

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No-Load Current Test indicates :

- Abnormal core grounds
- Winding faults: shorts, open circuits
- On Load Tap Changer problems
- Manufacturing defects
- Determines losses in the core (eddy current and hysteresis)





Execution of the test:

- Voltage applied on Primary side with Secondary side open circuit (in some countries vice versa)
- Current required to magnetize the core with Magnetic flux Ømag.
- This Magnetic flux induces the voltage V₂
- Current Required is the Excitation Current.







Significance of No Load Current Test:

• When a Load is placed on 2ry winding, a current will flow

 $|_2 = \frac{V2}{R2}$

- The current I2 will in-turn create an Opposing Magnetic Flux $\mathbf{Ø}_2$
- Considering the V₂ Voltage constant, the voltage generator V₁ will provide more current I₁ to maintain the core magnetized equal to the opposing flux

$$I_1 = I_{\text{excitation}} = I_{\text{mag}} + I_2$$



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Significance of No Load Current Test:

Turn-to- Turn Short circuit fault

- Any Shorted turns at Secondary side, will acts as a load across the fault winding which will leads to draw a fault current.
- The Excitation Current will increase in due to opposing flux created by the fault Øfault.
- ✓ Any short at Secondary Will result in increase Excitation Current.





Test to be performed :

- Each phase must be tested with the same voltage
- Test must be performed with highest Voltage possible
- Test Voltage must not exceed the Rated voltage
- Compare with Previous Results.





Up to 2kV @ 1.5A

Up to 12kV @ 300mA



Test Performed with 2kV voltage Source



SW recalculates to 10 kV



Test performed with accessory for Capacitance & Tandelta on a Star Winding Trafo



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Test performed with accessory for Capacitance & Tandelta on a Delta Winding Trafo



Note : Test is performed with Ungrounded specimen Test UST, Ground Current is bypassed.

12

No Load Current

Test Performed

- 400 kV / 132 kV Transformer
- Phase-Phase Comparison
- Shows two similar High Readings and one Low reading, it is common with 3 phase transformer

Excitation Current

6

Тар

8

10

1,2 ^{__}

2

4



Test Result Analysis

- Check the Phase to Phase : two similar high readings and one low reading is normal (though there are exceptions).
- When Tap Changers are present, consider the pattern within the phase.



In for this test, comparison of the results with the ones obtained in the factory is not suggested since the ones in factory were done with 3 ph source and usually a much higher voltage



SHORT CIRCUIT IMPEDANCE (Leakage Reactance)



"It the percentage of the nominal primary side voltage required to circulate full-load current under short circuit conditions on the secondary other side."

(Or)

The percentage impedance of a transformer is the voltage drop on full load due to the winding resistance and leakage reactance expressed as a percentage of the rated voltage.

Losses in Copper due to Ohm resistance of conductors (losses on a car due to its weight)

Z% = <u>Impedance Voltage</u> x 100 Rated Voltage



Why Short Circuit Impedance Test :

- To determines the maximum value of fault current that will flow under fault conditions
- It can show us possible winding movement caused by the heavy Fault Current that passed through the Transformer
- It can also show is possible Winding Deformation Caused during the transportation.

If we were to compare Transformer with a car, the car needs to «loose» some power to move its own mass. The same here, Trafo needs to loose some of the power to overcome its own ohmic resistance of the copper windings





How to Perform the Test :

- The test is conducted on the high-voltage (HV) side of the transformer.
- Low-voltage (LV) side or the secondary is short circuited (in some countries it is vice versa).
- Since Voltage Applied is Very low (e.g. 100 V) compared to the Rated Voltage, Core Losses are Neglected





How to Perform the Test :

- Watt Meter Reading Provides Watt Loss or Copper Loss.
- Result is compared With the Name plate Value **Z%** (e.g. 7.8 %, 10 %).
- Error Limit allowed maximum is 3% from Name Plate Value
- Use **Thick** cables to SC the secondary side





Testing on a 3 Phase Tansformer:

A three-phase transformer can be tested using a single-phase power source using one of these two Methods :

- 3 Phase Equivalent method (often used at the producer)
- Per Phase Method (if Primary is star winding, with neutral point accessible)
- In both case we will execute 3 measurements after which test set automatically shows us the result


Testing on a 3 Phase Transformer – 3 Phase equivalent method

Perform Test for :

H1-H2 H2-H3 H3-H1

Calculation for % Zk will be as below :



3-phase equivalent:

$$Zk \% meas = \frac{(Zk_{AB} + Zk_{BC} + Zk_{CA})[\Omega]}{60} \cdot \frac{P \text{ nominal } [kVA]}{V_{LL} \text{ nominal } [kV]}$$

Testing on a 3 Phase Transformer – Per Phase

Perform Test for :

H1-H0 H2-H0 H3-H0

Calculation for % Zk will be as below :

Per-phase:

$$Zk \ \% \ meas = \frac{Zk \ [\Omega]}{10} \cdot \frac{P \ nominal \ [kVA]}{V_{LL} nominal \ [kV]}$$







Data results		ts Graphica	al representat	ion											
P	Per-phase C		C 3-phase	e equivalent A	A-B 3-phase	equivalent B-(C 3-phase (equivalent C-/	A	4					
	#		f [Hz]	V [V]	Imax [A]	V meas [V]	φV [°]	I meas [V]	Loss [W]	^					
	1	V	15,0	56,000	1,000	28,686	83,8	1,003	3,105	Γ					
	2	V	30,0	100,000	1,000	59,332	86,5	1,043	3,777		lent B-C	3-phase e	quivalent C-A		4
	3		50,0	100,000	1,000	94,655	86,6	1,001	5,604		k [Ω]	Rk [Ω]	Lk [mH]		^
	4	V	75,0	100,000	1,000	120,471	87,6	0,852	4,210		447		0.000		
	5	V	135,0	100,000	1,000	99,929	87,6	0,395	1,638		,447	3,673	0,302		_
	6		200,0	100,000	1,000	99,946	87,5	0,268	1,185		,792	4,129	0,301	e	_
ŀ	7		300,0	100,000	1,000	115,581	87,3	0,208	1,139	+	,431	6,653	0,301	Θ	
ł										÷۲	1,282	6,895	0,300	0	
L	<						-,	-,	,	>	2,580	12,457	0,298	0	
						87,5	0,268	1,185	372,538	37	2,024	19,554	0,296	Θ	
						87,3	0,208	1,139	556,414	55	5,531	31,337	0,295	Θ	_ v
						<	1	1	1	1			1 1		>
			# Zk	% meas	Zk % no	om Dev	/ Zk %	Xk % me	as Xk	% N	lom	Dev Xk	%		
			1	17,112	16,	430	4,150	17,1	112		16,4	4,	150		



Meas	sures											
Data	result	s Graphical	representat	ion						_		
Per-	phase	A Per-phas	e B Per-ph	ase C 3-pha	ase equivalent	t A-B 3-pha	se equivalent	B-C 3-phas	e equivalent	C-A		
#		f [Hz]	V [V]	IMax [A]	Vmeas[V]	ΦV [°]	Imeas[A]	Loss [W]	Zk [Ω] Meas	Xk [Ω]		
1		50,0	100,000	1,000	10,996	84,2	1,000	1,116	11,002	10,945		
		Measures Data result	ts Graphica	l representat	tion		t A B - 2 ob		B.C. 2 abo		64	
		#	f [Hz]	V [V]	IMax [A]	Vmeas[V]	ΦV [°]	Imeas[A]	Loss [W]	Zk [Ω] Meas	Xk [Ω]	
		1 🜌	50,0	100,000	1,000	10,969	84,0	0,999	1,152	10,984	10,923	
#	Zk		Measure Data resu Per-phas	s Graphic se A Per-ph f [Hz]	al representat ase B Per-pl	tion hase C 3-ph IMax [A]	ase equivaler	nt A-B 3-phi ΦV [°]	ase equivalen Imeas[A]	t B-C 3-pha	se equivalent Zk [Ω] Meas	C-A Xk [Ω
		<		(50,0	100,000	1,000	11,082	83,8	1,000	1,192	11,079	11,015
			<									>
			# 2	zk % meas	Zk % non	n Dev Z	k % Xk	% meas	Xk % Nom	Dev Xk	%	
			1	8,282	5,00	00 6	5,639	8,282	5,0	65,0	539 💽	



FREQUENCY RESPONSE OF STRAY LOSSES (FRSL)



- **FRSL** is a Short Circuit Impedance Test , but the test at Variable Frequency i.e. 15Hz to 500Hz.
- It is the only electrical method to tell us about short-circuits between parallel strands and local overheating due to excessive eddy current losses.





- Short in Parallel Stands influence skin effect.
- The AC resistance Increases with the Increase in Frequency.



How to perform the Test :

- Test is similar to short circuit impedance test, but test is done at variable frequency.
- Results are interpreted by comparing phases





- Phase to Phase Comparison Showed that there is a problem with the transformer.
- Increase in Eddy current Loss increased in Ph A and Ph C resistance with Frequency., which indicates some local heating or short of copper laminations
- FRSL Test Advance which provides more information than short circuit impedance Test.







CAPACITANCE and TAN δ

34



- **C & TD test** is the most common technique used to asses the insulation of the Transformer.
- It is an AC test
- Test is used to check :
 - Mechanical Deformation.
 - Aging of the Insulation.
- Reference for wide range of insulation is always available for comparision.
- Test is performed always between two different Potentials.



Ideal (perfect) Insulation



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Actual Insulation

In a Real Insulation System there is also a loss current IR flowing in-phase with the voltage.

I Total **= IC + I**R





Actual Insulation



Tan Delta is the ratio of in-phase (resistive) current to the 90-degree (capacitive) current.

 $Tan \delta = IR / Ic$

Since Power dissipates due to IR

Tan Delta equals Dissipation Factor





Power factor (PF) is the ratio of resistive current to the total current.

For the δ value up to 10 °, PF and Tan Delta can be considered the same in value

 $\cos \phi = IR / I$ Total = $IR / Ic = Tan \delta$

I Total = IR+IC = IC (if δ is very small)

















Can be tested on all types of Transformers:

- Single Phase.
- Three Phase.
- Two Winding.
- Three Winding.
- Auto Transformers with Tertiary.
- Auto Transformer without Tertiary.
- Delta Winding.
- Star Winding.



Single Phase two winding Transformer





Three Phase two winding Transformer





Three Phase two winding Transformer





Three Phase Three winding Transformer





Test Results Tested by STS 5000 +TD5000.



[Test settings Te	mperature comp.				
	-Nominal values-					
	Cn	0,2000 nF	 Single 		GST 🔻	
	Τδn	50,000 µ	● <- V ->	v	2000,0 V	
	🗹 k	0,7640	● <- f ->	f	50,0 Hz	

Data results Graphical representation

- Tests										
#		Туре	Capacitance	Sweep	Mode	V [V]	^			
1 📝		HV Winding	СН	None	GST	20(
2	2 📝 HV		СН	CH Voltage						
<						>				
- Results										
#		V [V]	f [Hz]	Vout [V]	Iout [A]	Cp [F]	^			
1	V	2000,0	55,0	1987,3	12,932m	18,8297n				
2	V	4000,0	55,0	4007,9	26,089m	18,8347n				
3		6000,0	55,0	6010,3	39,123m	18,8346n				
4	V	8000,0	55,0	8010,3	52, 16 1m	18,8417n				
- م ا		10 Ok	55.0	9997 8	65 072m	18 8397n	~			







400 kV Transformer Bushing Capacitance Vs Voltage



Voltage Vs Capacitance



Transformer Bushing Frequency Vs Tandelta





Comparison Tan Delta (AC) vs. PI (DC) Test:

Tan Delta is:

- A) Less Destructive (DC leaves the free electrons that can cause PD if there were voids)
- B) Time Independent (Result of DC testing changes if the test duration changes)
- C) Faster
- D) Giving us more similar conditions (AC) than PI test since we are using the said equipment with AC voltage
- E) More repeatable
- F) Better because if we have a good and a bad layer, PI will show us accetable result, while Tan Delta will show us the real state of insulation



Capacitance tell us :

Capacitance provides the information of Deformation of the winding or partial breakdown with the bushing.

Tan δ tells about:

Ageing of insulation, contamination, moisture increase in the insulation.

DFR tan delta at low freq

Provides the information on the amount of water in the insulating material Frequencies go from mHz to kHz



SWEEP FREQUENCY RESPONSE ANALYSIS





Power transformer



Passive filter





Measurement transformer



Coil, motor, generator





Transformer is a combination of R, L and C



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SFRA

- Detectable defects with this test we will discover if something geometrically moved within the transformer as an effect of a hit to the transformer or as an effect of a very high current passing through the transformer
- Axial deformation of the winding
- Radial deformation of the winding
- Partial and localized deformation of a coil
- Short-circuit between turns
- Breaking a winding
- Connection problem (resistance, grounding, ...)
- Problem on the magnetic circuit







100 k

1 M

🔽 Log



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Radial deformation of the winding

Axial deformation of the winding

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- IEC 60076-18
- IEEE PC57.149/D8
- DLT911/2004
- CIGRE WGA2.26 & 342



CIGRE

- 1) End-to-End Open
- 2) End-to-End Short-Circuit
- Capacitive Inter-Winding (CIW)
- 4) Inductive Inter-Winding (IIW)

IEEE

Open Circuit Self Admittance (OC) Short Circuit Self Admittance (SC) Inter-Winding (IW) Transfer Admittance (TA)







Inductive inter-winding





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- IEC 60076-18
 - Measurement on max coil turn (winding + adjustment coil)
 - Measurement on nominal position of OLTC



	Test type	Test #	$3\phi \Delta - Y$ Group 2 $\theta \Rightarrow 30^{\circ}$ LAG	$3\phi Y-\Delta$ Group 2 $\theta \Rightarrow 30^{\circ}$ LAG	$3\phi \Delta - \Delta$ Group 1 $\theta \Rightarrow 0^{\circ}$	$3\phi Y-Y$ Group 1 $\theta \Rightarrow 0^{\circ}$	1 φ
	HV Open Circuit (OC)	1	H1-H3	H1-H0	H1-H3	H1-H0	H1-H2
	All Other Terminals Floating	2	H2-H1	H2-H0	H2-H1	H2-H0	(H1-H0)
		3	H3-H2	H3-H0	H3-H2	H3-H0	
	LV Open Circuit (OC)	4	X1-X0	X1-X2	X1-X3	X1-X0	X1-X2
	All Other Terminals Floating	5	X2-X0	X2-X3	X2-X1	X2-X0	(X1-X0)
		6	X3-X0	X3-X1	X3-X2	X3-X0	
	Short Circuit (SC)	7	H1-H3	H1-H0	H1-H3	H1-H0	H1-H2
	Short [X1-X2-X3] ^a	8	H2-H1	H2-H0	H2-H1	H2-H0	Short
		9	H3-H2	H3-H0	H3-H2	H3-H0	[X1-X2] ^a
	Capacitive Inter-Winding	10	H1-X1	H1-X1	H1-X1	H1-X1	H1-X1
	All Other Terminals Floating	11	H2-X2	H2-X2	H2-X2	H2-X2	
		12	H3-X3	H3-X3	H3-X3	H3-X3	
	Inductive Inter-Winding	13	H1-X1	H1-X1	H1-X1	H1-X1	H1-X1
	High (H) to Low (L)	14	H2-X2	H2-X2	H2-X2	H2-X2	Ground
	Ground (H- and X-) ^b	15	H3-X3	H3-X3	H3-X3	H3-X3	[H2, X2]
		-					
SFRA



• HV injection, LV open



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SFRA - Standard test dry transformer

• HV injection, LV open



SFRA - Frequecy resonnance test

Dry Transformer





SFRA - Standard & test plan



• HV injection, LV Short

Short circuit, no magnetisation current Measure the short circuit impedance The transfer function is the same for the 3 phases



SFRA - Standard & test plan

• LV injection, HV open









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• Comparison open and short measurement



Interpretation – We need to have the previous result (from the factory if we do this test for first time)

Software compares the new curve – transfer function - and the old one

If they match all is fine – focus is on extremes (maximums and minimums)

If they do not – something moved inside the PT



SFRA - When to perform this test



- Factory
 - Validation (quality, before and after short circuit test)
 - Before transformer transportation
- Commissioning
 - After transportation
 - After bushing and accessories assembled
- Exploitation
 - Insulation fault (Phase to ground, Phase to Phase)
 - Short-circuit (Phase to ground, Phase to Phase)
- Another
 - Earthquake
 - Lighting impulse



SFRA - When to perform this test





SFRA - Measurement analyze





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PARTIAL DISCHARGE ON THE TRANSFORMER

What is PD?





PD are micro sparks inside (Internal PD) or on the borders of different insulating materials (Surface PD) that show us that insulation start to degrade



- What is PD?
 - Local overheating of the transformer oil → hot spots → gasses → low density region → PD
 - Insulation (paper) damage caused by over voltages, lightning strikes
 - Manufacturing defects (sharp edges, bad impregnation,...)
 - Natural aging processes, humidity increase, ...
 - Contact wear in tap changers
 - Deposition of "conductive species" on transformer board
 - Faulty bushing taps
 - Selector problems (tap changer)

Partial Discharge



APPLICATIONS :

- Permanent Monitoring
 - Sensors
 - Acquisition Box
 - Communication & Alarms
- Quality Control in factory
- Spot PD measurements in the field
 - On-line service
 - Off-line service
 - Instruments



Sensors units used in PD measurment





Sensors units used in PD measurment





SPECIFICATIONS	
Voltage output @ 50Hz or 60Hz	1 ÷ 10Vrms
Max output transient voltage	90V _{peak}
V _{out} vs V _{in} phase shift	90°
Operating temperature	-25°C ÷ +65°C
Output connector	BNC
Protection degree	IP66
Current to ground @ 50Hz or 60Hz	Below 10mA

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Acquisition units used in PD measurment





Very advanced oscilloscopes with even more advanced software

Acquisition units used in PD measurment



Software needs to have ability to filter our the noise (since we measure very low values) and to separate the sources (corona, internal and surface PD)









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UHF External Sensor: 500MHz – 3GHz bandwidth



- UHF Spiral antenna is a sensor designed to receive electromagnetic (EM) emissions from a PD.
- It is a broadband antenna with a flat response. .
- It has been optimized to operate in a frequency range typical for PD activity and it was designed to provide maximum sensitivity and high gain.
- Its compact and robust design makes Spiral antenna the optimal sensor for direct installation on high voltage Transformers.
- It can be virtually applied in any electrical equipment provided that it has apertures or EM transparent surfaces.



HFCT 30mm / HFCT 50mm



HFCT clamp 39mm / HFCT clamp 140mm



If you decide to go for online monitoring of PD









If you decide to go for online monitoring of PD









Tap Adapter



TiScada software (On Virtual Machine)

- FO cable for communication purpose
- Coaxial cables inside protective pipe
- Power Supply cables



If you decide to go for online monitoring of PD



SYNOPTIC VIEW for a 3-phase TRANSFORMER





Many faults in the transformer lead to gaseous by-products dissolved in the oil. Therefore, a proper and regular dissolved gas analysis (DGA) is required to determine the status of the transformer.

A **DGA** is the first indicator of a problem and can identify:

- Deteriorating insulation and oil
- Overheating
- Hot spots
- Partial discharge
- Arcing

The "health" of the oil is a good indication of the "health" of the transformer.





Transformer Oil 'The Blood' of a Transformer

Transformers are filled with oil that cools and insulates its windings.

The insulating oil is in contact with the internal components, so as normal and abnormal events occur within the transformer, "fault gases" are produced and become dissolved in the oil.



Analyzing these gases provides a snapshot of the overall health of the transformer, much as a blood test provides a snapshot of the overall health of a human body.



Transformer Oil = 'The Blood' of a Transformer

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7	GASSES	DISSOLVED	IN THE OIL
Y	H2	CO	CH4
	Hydrogen	Carbon Monoxide	Methane
	C2H6	C2H4	C2H2
	Ethane	Ethylene	Acethylene
	02	CO2	N2
	Oxygen	Carbon Dioxide	Nitrogen
	H2O		
	Moistu	ure	

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- Different deterioration processes result in different DGA "fingerprints".
- Key gasses are formed by the degradation of oil: hydrogen (H₂), methane (CH₄), ethane (C₂H₆), ethylene (C₂H₄) and acetylene (C₂H₂) paper_carbon monoxide (CO), carbon dioxide (CO₂), oxygen (O₂), etc.
- Gas type and amount of gas are determined by the severity of the fault and the energy involved

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Standards involved with DGA

IEC 60567 ed4.0 (2011-10), Oil-filled electrical equipment – Sampling of gases and analysis of free and dissolved gases

IEC 60599 ed2.0 (1999-03), TC/SC 10, Mineral oilimpregnated electrical equipment in service - Guide to the interpretation of dissolved and free gases analysis

Cigré TB783 – (Oct 2019) DGA Monitoring. The different types and technologies of on-line gas monitors

<u>Accuracy</u> of the on-line monitors on the market Procedure for evaluating the <u>accuracy</u> of on-line gas monitors







For a DGA test the following condition ranges can be defined based on the severity of the fault (IEC60599, IEEE C57-104, ...):

C		Condit	ion ranges		primary cause
Gas	Good	Fair	Poor	Action	
Hydrogen (ppm)	<101	>100 <1000	>1000 <2000	>2000	pd, electrolysis of water
Methane (ppm)	<121	>120 <401	>400 <1001	>1000	overheated oil
Ethane (ppm)	<66	>64 <101	>100 <151	>150	overheated oil
Ethylene (ppm)	<51	>50 <101	>100 <201	>200	very overheated oil
Acetylene (ppm)	<36	>35 <51	>50 <81	>80	arcing in oil
Carbon Monoxide (ppm)	<351	>350 <571	>570 <1401	>1400	overheated paper, air polution
Carbon Dioxide (ppm)	<2501	>2500 <4001	>4000 <10001	>10000	overheated paper, atmosphere
Oxygen (ppm)	<3501	>3500 <7001	>7000 <10001	>10000	atmosphere





Understanding Fault Gases





Accurate fault identification methods – multiple gases







Rogers Ratios for Key Gases				
Case	R2 C ₂ H ₂ / C ₂ H ₄	R1 CH ₄ / H ₂	R5 C ₂ H ₄ / C ₂ H ₆	Suggested Fault Diagnosis
o	<0.1	>0.1 <1.0	<1.0	Unit normal
1	<0.1	<0.1	<1.0	Low-energy density arcing—PD (See NOTE)
2	0.1 3.0	0.1- 1.0	>3.0	Arcing—High-energy discharge
3	<0.1	>0.1 <1.0	1.0 3.0	Low temperature thermal
4	<0.1	>1.0	1.0 3.0	Thermal <700 °C
5	<0.1	>1.0	>3.0	Thermal >700 °C



Basic Fault Types Detectable with DGA

Code	Fault
PD	Partial discharges of corona type
D1	Discharges of low energy, including partial discharges of the sparking type
D2	Discharges of high energy
T1	Thermal fault T < 300 ºC
Т2	Thermal fault 300 °C < T < 700 °C
Т3	Thermal fault T > 700 °C
DT	Mixed electrical and thermal fault

Oil testing Lab

What we can offer?



Chlorinated Fluid Screen (Askarels, Wecosol, tri- and tetra-chlorobenzenes, perchloroethylene)

Screen, Chlorinated Fluid

Test	Method	
Water/RS	D 1533	
Neut. No.	D 974	
Furanic Compounds	D 5837	

Silicones

Screen, 5-Part Silicone		Screen, 6-Part Silico	Screen, 7-H	
Test	Method	Test	Method	Test
Color/Visual	D 2129, D 1524	Color/Visual	D 2129, D 1524	Color/Visu
Water/RS	D 1533	Water/RS	D 1533	Water/RS
Dielectric	D 877 or D 1816	Dielectric	D 877 or D 1816	Dielectric
Neut. No.	D 974	Neut. No.	D 974	Neut. No.
Spec. Gravity	D 1298	Spec. Gravity	D 1298	Spec. Grave
ti st.	10	Power Factor, 25°C	D 924	Power Fact

Test	Method
Color/Visual	D 2129, D 1524
Water/RS	D 1533
Dielectric	D 877 or D 1816
Neut. No.	D 974
Spec. Gravity	D 1298
Power Factor, 25°C	D 924
Power Factor, 100°C	D 924

Natural Esters

Test	Method
Color/Visual	D 1500, D 1524
Water/RS	D 1533
Dielectric	D 877 or D 1816 or D 1816 (2mm gap)
IFT	D 971
Neut. No.	D 974
Spec. Gravity	D 1298
Viscosity, 40°C	D 445
Power Factor, 25°C	D 924


Transformer Mineral Oil and High Molecular Weight Hydrocarbons

Method D 1500, D 1524

D 1533 D 1816

D 974

D 1298

Screen, Min	creen, Mini Screen, 4-Part/D 1816/PF		16/PF at 25°C
Test	Method	Test	Method
Water/RS	D 1533	Water/RS	D 1533
IFT	D 971	IFT	D 971
Inhibitor	D 2668	Dielectric	D 1816
Neut. No.	D 974	Pow. Factor, 25°C	D 924

Test	Method	
Water/RS	D 1533	
IFT	D 971	
Dielectric	D 1816	
Pow. Factor, 100°C	D 924	

Screen, Mini with PCB		Screen, 5-Part/D 1816	
Test	Method	Test	Meth
Water/RS	D 1533	Color/Visual	D 15
FT	D 971	Water/RS	D 15
nhibitor	D 2668	Dielectric	D 18
Neut. No.	D 974	Neut. No.	D 97-
PCB	D 4059	Spec. Gravity	D 12

Test	Method
Color/Visual	D 1500, D 1524
Water/RS	D 1533
Dielectric	D 877
Neut. No.	D 974
Spec. Gravity	D 1298

What we can offer?

Screen, 6-Part/D 877		Screen, 6-Part/D 1816	
Test	Method	Test	Method
Color/Visual	D 1500, D 1524	Color/Visual	D 1500, D 1524
Water/RS	D 1533	Water/RS	D 1533
Dielectric	D 877	Dielectric	D 1816
IFT	D 971	IFT	D 971
Neut. No.	D 974	Neut. No.	D 974
Spec. Gravity	D 1298	Spec. Gravity	D 1298

Test	Method
Color/Visual	D 1500, D 1524
Water/RS	D 1533
Dielectric	D 877
IFT	D 971
Neut. No.	D 974
Spec. Gravity	D 1298
Pow. Factor, 25°C	D 924

Test	Method
Color/Visual	D 1500, D 1524
Water/RS	D 1533
Dielectric	D 1816
IFT	D 971
Neut. No.	D 974
Spec. Gravity	D 1298
Pow. Factor, 25°C	D 924

Screen, 8-Part/D 1816

Test	Method
Color/Visual	D 1500, D 1524
Water/RS	D 1533
Dielectric	D 1816
IFT	D 971
Neut. No.	D 974
Spec. Gravity	D 1298
Pow. Factor, 25°C	D 924
Inhibitor or PF, 100°C	D 2668 or D 924

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What we can offer?

Screen, IEC	72
Test	Method
Color	ISO 2049, ASTM D 1500
Appearance	IEC 60296
Water/RS	IEC 60814
Dielectric	IEC 60156
IFT	ISO 6295, ASTM D 971
Acidity	IEC 62021
Dissipation Factor, 90°C	IEC 60247

Test	Method
Color/Visual	D 1500, D 1524
Water/RS	D 1533
Dielectric	D 877
Dielectric	D 1816
IFT	D 971
Neut. No.	D 974
Pour Point	D 97
Spec. Gravity	D 1298
Inhibitor	D 2668
Viscosity at 40°C	D 445
Pow. Factor, 25°C	D 924
Pow. Factor, 100°C	D 924
PCB	D 4059

Test	Method	Test
Color/Visual	D 1500, D 1524	Color
Water/RS	D 1533	Water
Dielectric	D 877	Diele
Dielectric	D 1816	Diele
IFT	D 971	IFT
Neut. No.	D 974	Neut.
Pour Point	D 97	Pour
Spec. Gravity	D 1298	Spec.
Inhibitor	D 2668	Inhibi
Viscosity at 40°C	D 445	Visco
Pow. Factor, 25°C	D 924	Pow.
Pow. Factor, 100°C	D 924	Pow.
PCB	D 4059	PCB
Flash Point	D 92	Disso
Aniline Point	D 611	Partic
Corrosive Sulfur	D 1275B	Partic
PFVO	Doble	Corro
SFL	Doble	Sulfu
		Furan

Test	Method
Color/Visual	D 1500, D 1524
Water/RS	D 1533
Dielectric	D 877
Dielectric	D 1816
IFT	D 971
Neut. No.	D 974
Pour Point	D 97
Spec. Gravity	D 1298
Inhibitor	D 2668
Viscosity at 40°C	D 445
Pow. Factor, 25°C	D 924
Pow. Factor, 100°C	D 924
PCB	D 4059
Dissolved Metals	D 5185
Particulate Metals	Doble
Particle Count	D 6786
Corrosive Sulfur	D 1275B
Sulfur, CCD Test	Doble
Furanic Compounds	D 5837



What we can offer?

Specification Testing

Test	Method	Test	Method	Test	Method
Aniline Point	D 611	Aniline Point	D 611	Viscosity, 40°C	ISO 3104
Color	D 1500	Color	D 1500	Viscosity, -30°C	ISO 3104
Visual	D 1524	Visual	D 1524	Pour Point	ISO 3016
Flash Point	D 92	Flash Point	D 92	Moisture	IEC 60814
IFT	D 971	IFT	D 971	Dielectric, received	IEC 60156
Pour Point	D 97	Pour Point	D 97	Dielectric, after filtering	IEC 60156
Spec. Gravity	D 1298	Spec. Gravity	D 1298	Density, 20°C	ISO 3675, ISO 12185
Viscosity at 100°C	D 445	Viscosity at 100°C	D 445	Dissipation Factor, 90°C	IEC 60247
Viscosity at 40°C	D 445	Viscosity at 40°C	D 445	Appearance	IEC 60296
Viscosity at 0°C	D 445	Viscosity at 0°C	D 445	Acidity	IEC 62021
Dielectric	D 877	Dielectric	D 877	IFT	ISO 6295
Dielectric	D 1816	Dielectric	D 1816	Total Sulfur	ISO 14596
Impulse Breakdown	D 3300	Impulse Breakdown	D 3300	Corrosive Sulfur	DIN 51 353
Gassing Tendency	D 2300	Gassing Tendency	D 2300	Antioxidant	IEC 60666, Sec. 5.1
Power Factor, 25°C	D 924	Power Factor, 25°C	D 924	2-Furfural	IEC 61698
Power Factor, 100°C	D 924	Power Factor, 100°C	D 924	Oxidation Stability	IEC 61125C
Oxidation Stability	D 2440	Oxidation Stability	D 2440	Gassing Tendency	IEC 60628
Oxidation Stability	D 2112	Oxidation Stability	D 2112	Flash Point	ISO 2719
Inhibitor	D 2668	Inhibitor	D 2668	PCA Content	IP 346
Corrosive Sulfur	D 1275B	Corrosive Sulfur	D 1275B	PCB Content	IEC 61619
Water/RS	D 1533	Water/RS	D 1533		
Neut. No.	D 974	Neut. No.	D 974	Optional Tests	
PCB Content	D 4059	PCB Content	D 4059	ECT Test	CIGRE SC12
Furanic Compounds	D 5837	Spread of the second	11000000000000000000000000000000000000	Baader Test	DIN 51 554
PFVO	Doble			CCD Test	IEC 62535
SFL	Doble				
Carbon Type	D 2140				
Doble CCD Test	Doble				
Dibenzyl Disulfide	Doble				
Benzotriazole	Doble				
Irgamet 39	Doble				



What we can offer?

TEST	Method	Amount
Copper Content in Insulating Paper or Pressboard	Doble	5 grams
Corrosive Sulfur in Oil (Copper Strip)	ASTM D 1275A or B	250 mL
Corrosive Sulfur in Oil (Silver Strip)	DIN 51 353	150 mL
Corrosive Sulfur in Oil (Copper Strip), discontinued	ISO 5662	250 mL
Covered Conductor Deposition, Doble	Doble	50 mL
Covered Conductor Deposition and Dielectric Strength of Paper	Doble	50 mL
Covered Conductor Deposition	IEC 62535	50 mL
Covered Conductor Deposition, ABB	ABB	50 mL
Dibenzyl Disulfide	Doble	5 mL
Elemental (free) Sulfur	UOP-286/387	80 mL
Inorganic Chlorides and Sulfates	ASTM D 878	100 mL
Mercaptan Sulfur	ASTM D 3227	50 mL
Passivator Determination (BTA/Irgamet 39®)	Doble	10 mL
Pilot Treatment for Removal of Corrosive Sulfur Compounds	Doble	1 to 2 liters
Treatment Experiments to Remove Corrosive Sulfur (other than above)	Doble	1 to 2 liters
SEM/EDX of Copper, Paper or other solids	Doble	Contact lab
Sulfur Content in Insulating Paper or Pressboard	Doble	5 grams
Corrosive Sulfur Presence in Insulating Paper or Pressboard with silver	Modified TAPPI T 444	100 cm^2
Sulfur Speciation	ASTM D 5623	30 mL
Tamish Level of Copper Strip used in corrosive sulfur tests	ASTM D 130	N/A
Total Sulfur	ASTM D 4294 ISO 14596	10 mL



What we can offer?

Individual Tests for Mineral Oil TEST	ASTM Number	Volume of* Liquid, mL
Dissolved Gas-in-oil analysis (DGA)	D 3612A or C	35
Color	D 1500	50
Dielectric Breakdown	D 877A or B	80
Dielectric Breakdown	D 1816	450
Furanic Compounds in Oil	D 5837	20
Inhibitor Content	D 2668	1
Interfacial Tension	D 971	25
Neutralization Number	D 974	20
Polychlorinated Biphenyls (PCBs) in Oil	D 4059	5
Power Factor @ 25°C	D 924	250 (1 liter**)
Power Factor @ 100°C	D 924	250 (1 liter**)
Power Factor @ 25°C & 100°C	D 924	250 (1 liter**)
Specific Gravity	D 1298	500
Viscosity @ 40°C	D 445	25
Visual Examination	D 1524	300
Water Content – Oil	D 1533	10



Brakedown voltage – We put oil in a small standardizrd holder – tank – and we apply voltage with fixed distance between electrodes

At one point in time (as we increase the voltage between electrodes) the oil will become conductive – there will be a spark between electrodes We note that number and see if it is lower than allowed

DC Voltage testing

An older metod

Today we prefer to use TD (DF,PF) which is AC testing Makes sense on PT with solid insulation while PT with liquid insulation will not have repeatable results (oil moves within the PT)

We generate certain voltage (5 kV) to measure what is called the Polarization Index, or PI, which is a ratio of the megohms after 10 minutes divided by the megohms after 1 minute

Less than 1	Dangerous	
10 – 1.1	Poor	
1.1 – 1.25	Questionable	
1.25 – 2.0	Fair	



DC Voltage testing



Dielectric Absorption Ratio (DAR)

Ratio of the megohms at 1 minute divided by the megohms at 30 seconds. When the measured leakage current stabilizes within 1 minute, operators typically use the DAR Test.

If this happens, the 10 minute PI test is useless because the ratio is 1. Values for DAR and PI commonly used in the literature and by manufacturers of test equipment for assessing the insulation conditions are:





Offline testing of underground cables with high level intro - APAC

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A CAR DO

Las diferentes herramientas de diagnóstico del Análisis de Gases Disueltos (DGA), cuándo / cómo usarlas de manera eficiente



Mag Managing and visualizing transformer oil test data - EMEA





Managing and visualizing transformer oil test data - APAC



Thank you for your attention ©

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